

# THE EFFECT OF THE ACCELERATOR POSITION ON THE FUEL CONSUMPTION OF ROAD VEHICLES

Ing. Tomáš Skrúčaný<sup>1</sup>, Ing. Branislav Šarkan, PhD<sup>2</sup>., doc. Ing. Juraj Jagelčák, PhD.<sup>3</sup>

University of Zilina, Department of Road and Urban Transport, Slovakia<sup>1,2,3</sup>

tomas.skrucany@fpedas.uniza.sk<sup>1</sup>

branislav.sarkan@fpedas.uniza.sk<sup>2</sup>

juraj.jagelcak@fpedas.uniza.sk<sup>3</sup>

**Abstract:** The fuel consumption of road vehicles is influenced by many factors. One of them is the accelerator position. Measurement of the fuel consumption on a rollingstand was done for the quantification of this effect. The tested vehicle was Kia Cee'd with a petrol engine. The measurements were done in laboratory conditions to give higher accuracy. The results describe the degree of the effect of the accelerator position. They can be used for the determination the position considering to the actual output power of the engine and for the determination of the correctly driver behaviour. The correctly usage of the accelerator contributes to the reduction of environmental burden of transport.

**Keywords:** ACCELERATOR POSITION, OUTPUT POWER, FUEL CONSUMPTION

## 1. Introduction

One of the most common bad behaviors of drivers is incorrect usage of the accelerator. His actual position is influencing the fuel consumption. With the decreasing of the distance between the accelerator and the floor, the fuel consumption is increasing very fast and the vehicle's acceleration is increasing slower. This effect is higher with increasing ratio of the acceleration position.

## 2. Measurement

The measurement was done on the rollingstand. This equipment allowed to simulate different driving modes with high accuracy. So it is able to simulate vehicle's drive at a constant speed, uphill driving, acceleration or the mixture of them. The rollingstand MAHA LPS 2000 with external equipment – engine speed sensor. Except of the driving modes simulations, the rolling stand can measure the maximal wheel power, engine effective (output) power, velocity and torque.

For the measurement of the fuel consumption was used Flowtronic. This equipment measure the volume of the flowing liquid fuel (petrol) on the principle of the rotating pistons with rated volume.

For the monitoring of the throttle position was used diagnostic unit Kia HiScan. This unit can be connected to the OBD port. It is measuring and visualising all operational data of the engine. It can be used only in the vehicles of the mark Kia.

The tested vehicle was Kia Cee'd with petrol engine of the volume 1,6 l, the output power 90 kW.

The rollingstand, other equipment, the vehicle and laboratory are the property of the Department of the Road and Urban Transport at the University of Zilina.



Fig. 1 Rollingstand in the laboratory.

## 3. Vehicle dynamic specifications

As the basic point of the output power which is needed to reach standard driving dynamic, it is necessary to terminate what is „the standard“. This standard driving and dynamic situations are:

1. Driving at a constant speed (according to the conditions – urban area, extra-urban area, motorway)
2. Acceleration needed to reach a constant speed (according to the regulation ECE 101).

### 3.1. Driving power equations:

#### Rolling resistance:

$$(1) \quad P_f = G_T \cdot \cos \alpha \cdot f \cdot v = m \cdot g \cdot \cos \alpha \cdot f \cdot v [W]$$

$m$  – vehicle weight [kg],  $g$  – gravity acceleration [ $m \cdot s^{-2}$ ],  $\alpha$  – elevation angle [ $^\circ$ ],  $f$  – rolling coef. [-],  $v$  – velocity [ $m \cdot s^{-1}$ ]

#### Aerodynamic drag:

$$(2) \quad P_v = \frac{1}{2} \cdot \rho_v \cdot c_d \cdot S \cdot v^3 [W]$$

$\rho_v$  – air density [ $kg \cdot m^{-3}$ ],  $c_d$  – drag coef. [-],  $S$  – frontal area [ $m^2$ ]

#### Elevation:

$$(3) \quad P_s = G_T \cdot \sin \alpha \cdot v = m \cdot g \cdot \sin \alpha \cdot v [W]$$

**Acceleration:**

$$(4) \quad P_a = m \cdot a \cdot \delta \cdot v \quad [W]$$

*a* – driving acceleration [m.s<sup>-2</sup>], *δ* – rotating masses coef [-]

**Summary of wheelpower:**

$$(5) \quad P_k = P_e \cdot \eta_P = \Sigma P = P_f + P_v + P_s + P_a \quad [W]$$

*P<sub>k</sub>* – wheelpower [W], *P<sub>e</sub>* – engine output power [W], *η<sub>P</sub>* – gear efficiency [-]

The summary are considered for individual driving modes:

1. Constant speed, no elevation

$$P_1 = P_e \cdot \eta_P = \Sigma P = P_f + P_v \quad [W]$$

2. Constant speed with elevation

$$P_2 = P_e \cdot \eta_P = \Sigma P = P_f + P_v + P_a \quad [W]$$

3. Acceleration (only without elevation)

$$P_3 = P_e \cdot \eta_P = \Sigma P = P_f + P_v + P_a \quad [W]$$

**3.2. Input vehicle values**

*m* = 1518 kg (1263 kg empty vehicle + 3 persons á 75 kg and 30 kg luggage)

*f* = 0,01

*c<sub>d</sub>* = 0,32

*S* = 2,05 m<sup>2</sup>

*δ* = 1,05 – 1,11 (according to the actual gear)

*η<sub>P</sub>* = 0,93

- Other factors are considered with values in reference physical conditions

For the calculation of „normal driving power values“ was necessary to set casual acceleration and velocity values. Velocity at constant speed was chosen as border or round values used in cities, local roads or highways. For the set of acceleration was chosen as basic the values used in the ECE Vehicle Regulation n. 101.

**Table 1: Acceleration values**

Our values		Reg. No. 101		
Velocity (km.h <sup>-1</sup> )	Acceleration (m.s <sup>-2</sup> )	Acceleration (m.s <sup>-2</sup> )	Velocity (km.h <sup>-1</sup> )	Cycle
15-30	0,8	0,79	(15-32)	urban cycle
30-50	0,5	0,45	(35-50)	urban cycle
50-70	0,45	0,4 - 0,43	(50-70)	urban cycle
70-90	0,25	0,24	(70-100)	extra-urban
90-110	0,25	0,24	(70-100)	extra-urban
110-130	0,3	0,28	(100-120)	extra-urban

**Table 2: Engine output power**

Engine output power (kW)							
Mode	Elevation (%)	Velocity (km.h <sup>-1</sup> )					
		30	50	70	90	110	130
Constant speed	0	1,6	3,4	7,1	12,4	20,2	31,1
	3	5,6	10,1	16,4	24,4	34,9	48,5
	6	9,6	16,7	25,7	36,3	49,5	-
	9	13,6	23,4	35,0	48,3	-	-
	12	17,5	29,9	44,2	60,1	-	-
	15	21,4	36,4	53,2	71,8	-	-
Acceleration	Acceleration (from - to, velocity)						
	15 - 30	30 - 50	50 - 70	70 - 90	90 - 110	110 - 130	
	13,6	16,0	22,4	23,2	33,4	46,6	

Table 2 describes the engine output power calculated according to the equations of the driving power (Eq.1 - 5). The red numbers are the border values, which occur infrequently during normal operation. The elevation values and the velocity were set according to the border or round values. E.g. the elevation 6% is usually at local roads where is the speed limit 90 km/h, but it is rather an exception on highways. So it is not necessary to consider with output power in these columns (-). The power values during accelerations were set as the largest value of the output power in the corresponding interval.

**4. Accelerator position and fuel consumption**

**Table 3: Accelerator position and output power**

Throttle position (%)	Accelerator position (%)	Engine output power (kW) at rpm					
		2100	2500	2700	3300	3500	3900
78,8	100	29,7	35,6	40,1	48,7	51,9	59,6
32,2	41	26,7	32,1	36,0	43,8	46,7	53,7
20	25	24,0	28,9	32,4	39,4	42,0	48,3
16,1	20	21,4	25,7	28,9	35,2	37,5	43,1
13,7	17	17,9	21,5	24,2	29,4	31,3	36,0
11,4	14	14,6	17,5	19,6	23,9	25,5	29,2
10,2	13	12,4	14,9	16,8	20,4	21,8	25,0
9	11	9,9	11,8	13,3	16,2	17,2	19,8
7,8	10	7,7	9,2	10,3	12,6	13,4	15,4
6,7	9	5,5	6,6	7,4	8,9	9,5	11,0

This table describes the most often used output power and operational engine rotation. These values were calculated according to the previous table. The colour of each column represents driving mode and corresponding elevation from the previous table. This calculated power occurs during the vehicle operation described in the previous tables.

Throttle position was identified through HiScan diagnostic. It is necessary to note, that the accelerator position and the throttle position are not the same values.

The table shows the area of the accelerator position used during the „normal“ operation. The operational range of the accelerator is in the interval of 0 – 40 % of its whole range. It seems that every position out of this interval is unnecessary, because the output power increases very slowly (see fig. 1), but the fuel consumption considerably (see fig. 2).

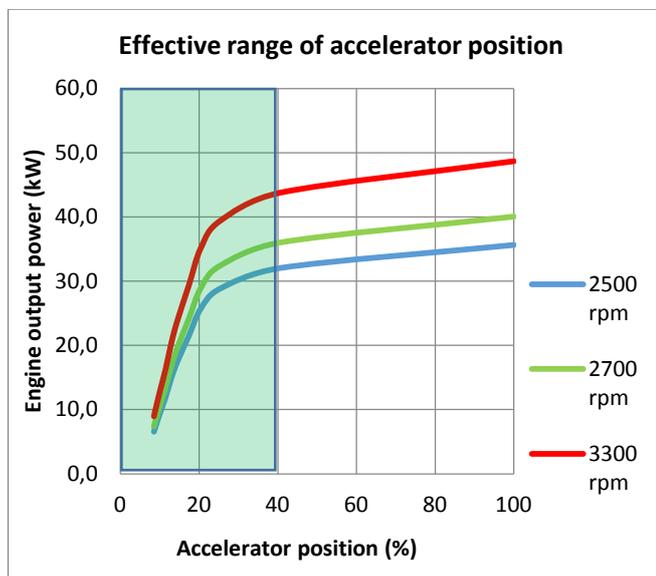


Fig. 2 Effective range of the accelerator position

Figure 2 shows the increasing output power according to the accelerator position (0% is idle, 100% is kick down). The output power values and increasing characteristics in the interval up to 40 % is optimal for the vehicle operation.

Table 4: Accelerator position and fuel consumption

Accelerator position (%)	Fuel consumption (l/100km)	Output power (kW)
100	25,76	35,6
41	21,09	32,1
25	19,96	28,9
20	15,29	25,7
17	13,84	21,5
14	11,43	17,5
13	9,98	14,9
11	8,37	11,8
10	7,08	9,2
9	7,89	6,6

Table 4 shows the characteristic the fuel consumption according to the accelerator position. The right column represents the output power needed to drive the vehicle at the velocity 50 km.h<sup>-1</sup> (colouration to the elevation and acceleration). The blue square borders the output power needed to the acceleration to the velocity 50 km.h<sup>-1</sup>. The fuel consumption values are results of the fuel consumption measurement done at engine speed of 2500 rpm using the 3<sup>rd</sup> gear which corresponds the velocity 50 km.h<sup>-1</sup>.

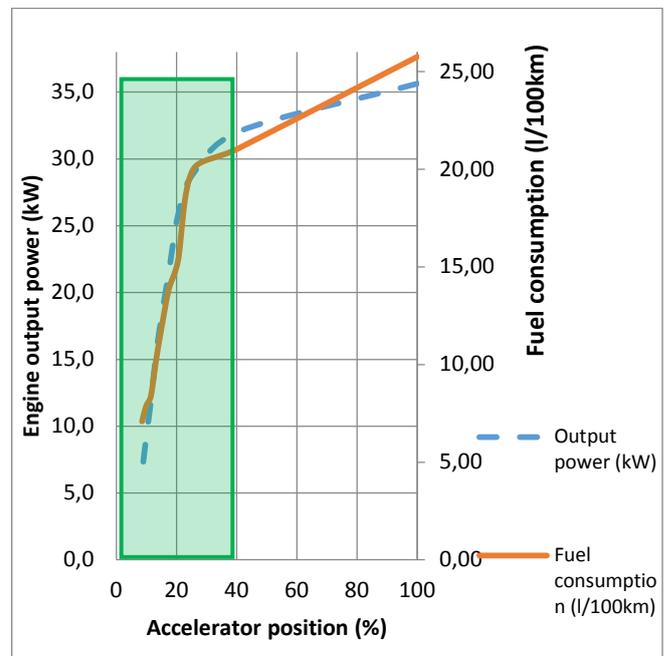


Fig.3 Course of the fuel consumption and the output power

### 5. Conclusion

The results point to the fact to mind during driving. It is the reality that accelerator position does not correspond with the engine output power, vehicle dynamics and fuel consumption. During the accelerator pushing down (from the idle to the kick down), the output power is increasing less and the fuel consumption is increasing more. The optimal operational range of the accelerator is up to 40% of the total range. Over this interval is the vehicle operation less effective from the economic and environmental point.

### 6. Literature

[1] Šarkan B., Skrúčaný T., The issue of measuring the fuel consumption of road freight vehicles with a volumetric flowmeter [Problematika merania spotreby paliva cestných nákladných vozidiel objemovým prietokomerom]/In: Machines, technologies, materials [elektronický zdroj] = MTM : international virtual journal. - ISSN 1313-0226. - 2013. - Vol. 7 , no. 8 (2013), online, s. 36-39., trans & MOTAUTO '13 [elektronický zdroj] : XXI international scientific and technical conference on transport, road-building, hoisting transportation engineering and technology : 01.-02.07 2013 - Varna, Bulgaria : proceedings. - [S.l. : s.n.], 2013. - ISSN 1310-3946. Year 21, no. 7, 8, 9/144/145/146 (2013), CD-ROM, [4] s

[2] V. Rievaj, A. Kalašová, J. Rievaj., Fuel consumption and driving resistances [Spotreba automobilu a jazdné odpory] / In: Archives of transport system telematics. - ISSN 1899-8208. - Vol. 5, iss. 2 (May 2012), s. 32-36.

[3] Branislav Šarkan, Ján Vrábek., Modification of the engine control unit and its impact on fuel consumption and vehicle performance [Úprava riadiacej jednotky motora a jej vplyv na spotrebu paliva a výkonvozidla]/In: Doprava a spoje [elektronický zdroj] : internetový časopis. - ISSN 1336-7676. - 2012. - Č. 2 (2012), online, s. 375-380.

[4] ECE Regulation No. 661/2009

[5] ECE Regulation No. 1222/2009

[6] ECE Regulation No. 101