

# EFFECT OF TREATMENT TEMPERATURE OF TiO<sub>2</sub>/SiO<sub>2</sub> AND ZrO<sub>2</sub>/SiO<sub>2</sub> COATINGS ON THEIR CORROSION STABILITY

Assist. Prof. St.Yordanov PhD.<sup>1,\*</sup>, Assoc. Prof. I. Stambolova PhD<sup>2</sup>, Assoc. Prof. V. Blaskov PhD<sup>2</sup>, Prof. L. Lakov PhD<sup>1</sup>,

Prof. S. Vassilev PhD<sup>3</sup>, Asst Y. Kostova<sup>1</sup>, M. Assoc. Prof. B.Jivov PhD<sup>1</sup>

E-mail: stancho14@abv.bg

Bulgarian Academy of Sciences, Institute of Metal Science, Equipment and Technologies with Hydro- and Aerodynamics Centre "Acad. A. Balevski", Sofia, Bulgaria<sup>1</sup>,

Institute of General and Inorganic Chemistry, Bulgarian Academy of Sciences, Bulgaria<sup>2</sup>,

Institute of Electrochemistry and Energy Systems, Bulgarian Academy of Sciences, Acad. G. Bonchev St., bl. 10, 1113 Sofia, Bulgaria<sup>3</sup>

**Abstract** Titanium dioxide coatings and zirconium dioxide were deposited on SiO<sub>2</sub> underlayers by sol-gel method on stainless steel plates. The samples were treated at two different temperatures (500 and 700°C) in air. The morphology was examined by means of Scanning electron microscopy (SEM) and the phase composition by X-ray diffraction analyses. The corrosion resistance of the coatings were examined by evaluation of the weight loss in NaCl medium. The TiO<sub>2</sub>/SiO<sub>2</sub> coatings possess relatively smooth surface with some crystallites on the surface, while ZrO<sub>2</sub>/SiO<sub>2</sub> coatings are not so smooth. After treatment at higher temperature the ZrO<sub>2</sub>/SiO<sub>2</sub> coatings become rougher. The weight loss measurement have proved that the TiO<sub>2</sub>/SiO<sub>2</sub> coatings exhibit higher corrosion resistance in comparison to ZrO<sub>2</sub>/SiO<sub>2</sub> coatings. The TiO<sub>2</sub>/SiO<sub>2</sub> coatings, treated at 500°C after the corrosion test retain their characteristic grain structure without any cracks and other defects. Similar is the structure of these coatings, treated at 700°C. The better protective properties of TiO<sub>2</sub>/SiO<sub>2</sub> could be attributed to their amorphous dense structure.

**Keywords:** SOL-GEL, MULTILAYERS, NANOSIZED FILMS, BARRIER PROPERTIES, FILMS

## 1. Introduction

Corrosion can be defined as a chemical or electrochemical reaction between a material, usually a metal, which has many serious economic, health, safety etc consequences. There are several methods of corrosion control: inhibitors, cathodic protection and applying of coatings. Coatings for corrosion protection can be divided into two broad groups - metallic and nonmetallic (organic and inorganic). [1,2] Recently, the inorganic oxide coatings are increasingly used for range of industrial applications to provide wear and erosion resistance, thermal insulation and corrosion protection [3]. Among them, ZrO<sub>2</sub> coatings have good chemical and thermal stability, high strength, high dielectric constant etc., which make them suitable for anticorrosion coating for steels protection [4]. Titania coatings are also widely used as anticorrosion coatings on stainless steel [5-7]. The physical and chemical properties of the both ZrO<sub>2</sub> and TiO<sub>2</sub> films strongly depend on the deposition method and the corresponding heat treatment process, especially the temperature of thermal treatment [8]. Multilayer coatings have recently been increasingly used as anticorrosive coatings because they provide better protective properties compared to monolayer coatings. [9] The multilayer configuration of the two types of oxides applied to each other has the combined effect of their advantages, and the surface layer to protect the parent metal should have increased corrosion resistance. The aim of this article is to study the effect of the heating temperature of ZrO<sub>2</sub> and TiO<sub>2</sub> nanosized coatings, deposited over silica sol gel layers to their corrosion resistance.

## 2. Experimental

The silica underlayers were prepared from tetraethoxyl silane (TEOS) dissolved in a mixture of ethanol, water and hydrochloric acid as a catalyst. The molar ratio H<sub>2</sub>O: TEOS is 3.7. The solution undergoes aging for 7 days. Stainless steel AISI 316 7.5x 2.5 cm were cleaned ultrasonically in ethanol and acetone, after that were immersed in the solution and withdrawn at a constant rate of 3 cm / min and then dried at 60°C and at

90°C and finally at 300°C. These steps are repeated two times. In ZrO<sub>2</sub>/SiO<sub>2</sub> (SZ) samples were deposited three ZrO<sub>2</sub> layers over SiO<sub>2</sub> layers, using ZrOCl<sub>2</sub>.8H<sub>2</sub>O with a acetylacetone and then dried sequentially at 300°C. The dipping-drying steps were repeated 3 times, finally was carried out final treatment at 500°C or 700°C (sample code SZ5 and SZ7, respectively). The same procedure was applied for the preparation of TiO<sub>2</sub> /SiO<sub>2</sub> samples with codes ST5 and ST7. The TiO<sub>2</sub> coatings were deposited from precursor titanium isopropoxide Ti (OC<sub>3</sub>H<sub>7</sub>)<sub>4</sub> (98%), dissolved in a mixture of ethanol and butanol . The phase compositions of the samples were studied by X-ray diffraction (XRD) with CuK $\alpha$ -radiation (Philips PW 1050 apparatus). A scanning electron microscope (SEM) Philips 515 was used for morphology observations of the films. The chemical corrosion resistance of the investigated samples and uncoated stainless steel (reference sample) were studied by immersion in salty corrosive solution of 3.5% NaCl at 25°C (EN ISO10289/2006) for 200 hours .The temperature of solution and the air temperature were controlled by calibrated thermometers.

## 3. Results and discussion

The figure 1-a indicates the presence of orthorhombic crystallographic phase of ZrO<sub>2</sub> and SiO<sub>2</sub> phase in sample SZ5 with crystallites sizes 44 and 75 nm , respectively. After heating at 700°C the sample SZ7 crystallizes in cubic ZrO<sub>2</sub> phase with very fine crystallites (9 nm) (Fig 1b). The X-ray diffraction patterns of sample ST5 heated at 500°C do not indicate the presence of a crystalline phase of TiO<sub>2</sub>, i.e. the sample has amorphous structure (Fig 1-c) During the isothermal heating at 700°C both phases are formed: nanocrystalline anatase phase TiO<sub>2</sub> phase and SiO<sub>2</sub> phase. The same result was obtained from Cheng and co-authors for sol gel SiO<sub>2</sub> doped titanium dioxide films [10]. They have proved that the peaks intensity of the anatase phase is weakening with an increase in silica concentration and the films doped with 20% SiO<sub>2</sub> is amorphous. Another group of researchers also showed that the introduction of SiO<sub>2</sub> into TiO<sub>2</sub> nanoparticles suppress the crystallization of the anatase phase [11].

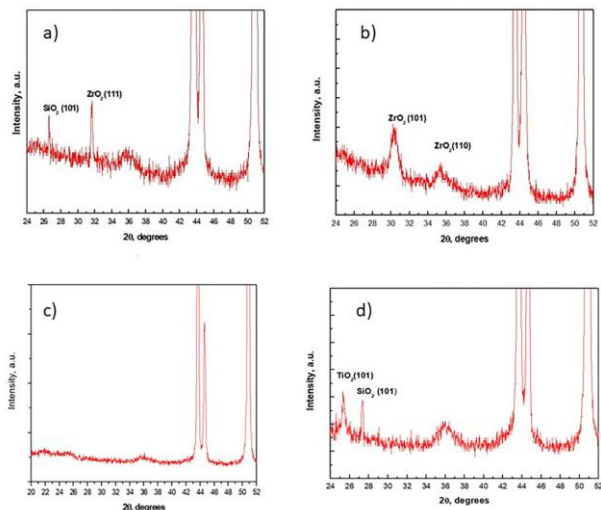


Fig. 1 XRD patterns of the  $\text{TiO}_2$  and  $\text{ZrO}_2$  coatings on silica underlayers: SZ5 (a), SZ7 (b), ST5 (c) and ST7 (d)

The morphology of multi-layered  $\text{ZrO}_2$  and  $\text{TiO}_2$  coatings on silicon dioxide: freshly prepared and after the corrosion test is presented on figures 2 and 3. The coatings  $\text{SiO}_2/\text{ZrO}_2$  are relatively thick with the presence of nanosized pores (Fig 2). The surface of ST sample is relatively dense with a few surface nanocrystals of different sizes. (Figure 3a) There are no visible cracks and pores. After thermal treatment at  $700^\circ\text{C}$  more numerous larger superficial nanocrystals are observable (Figure 3b). After the corrosion test the roughness of titania coatings deposited on  $\text{SiO}_2$  treated at lower temperature increases slightly without showing any effects of corrosion such as cracks and other defects (Figure 3c). The corrosive attack deteriorates significantly the surface of the samples, treated at  $700^\circ\text{C}$  (not shown here).

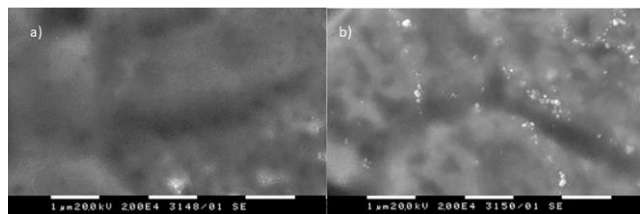


Fig. 2 Morphology of the SZ5 (a) and SZ7 coatings (b)

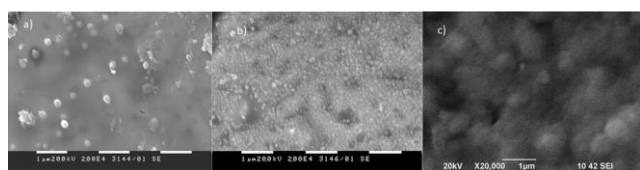


Fig. 3 Morphology of ST5 (a) and ST7 coatings (b) and after corrosion test : ST5 (c)

As it can be proved by evaluation of mass of the samples after immersion in saline medium,  $\text{TiO}_2$  on  $\text{SiO}_2$  multilayers exhibit improved corrosion resistance in comparison with those of the  $\text{ZrO}_2/\text{SiO}_2$ . The best barrier properties were shown by  $\text{TiO}_2/\text{SiO}_2$  underlayers, heated at  $500^\circ\text{C}$ . Zero weight loss was registered after 200 hours of corrosion test for these coatings. The  $\text{TiO}_2/\text{SiO}_2$  coatings treated at higher temperature have shown slightly weaker protective properties. Increased temperature of treatment of these  $\text{ZrO}_2/\text{SiO}_2$  samples lead to strong increase of corrosion rate.

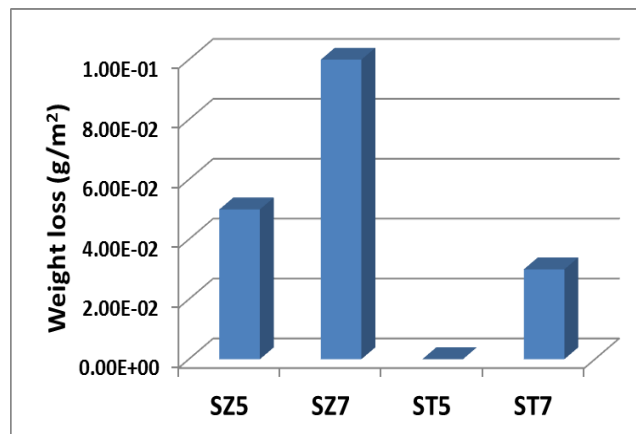


Fig. 4 Weight loss of the multilayer samples  $\text{ZrO}_2/\text{SiO}_2$  and  $\text{TiO}_2/\text{SiO}_2$ , treated at two different temperatures

It was established by other research group that the presence of amorphous structure of  $\text{TiO}_2\text{-SiO}_2$  composite deteriorates the ion and electron conduction of the films, thus acting positively on the corrosion protection [12]. The relatively dense, amorphous structure of the samples  $\text{TiO}_2/\text{SiO}_2$ , may be reason for their better protective properties than those of the  $\text{ZrO}_2/\text{SiO}_2$  multilayers.

#### 4. Conclusions

Coatings, consisting of  $\text{TiO}_2$  and  $\text{ZrO}_2$  deposited over  $\text{SiO}_2$  underlayers were obtained by dipping technique. The titania coatings on silica underlayer are relatively smooth with many crystallites on the surface, while the  $\text{ZrO}_2/\text{SiO}_2$  coatings are rougher. The  $\text{TiO}_2$  coatings on  $\text{SiO}_2$  treated at lower temperature manifested the higher corrosion resistance than that of  $\text{ZrO}_2$  samples, which have been proved from the weight loss test in NaCl medium and the morphology studies. The increasing of the treatment temperature deteriorates the protection properties of the both types of coatings. The better protective properties of  $\text{TiO}_2/\text{SiO}_2$ , heated at  $500^\circ\text{C}$ , could be attributed to their amorphous structure and relatively dense surface. The obtained new multilayer structures are promising with the view to increase the corrosion resistance of the steel and this fact gives us the reason to extend the scope of the experiments.

#### 5. Acknowledgements

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#### 6. References

- I.E.W. Brooman, Modifying organic coatings to provide corrosion resistance Part III: Organic additives and conducting polymers, *Met. Finish*, 100 (2002) 104-110
- S. K. Tiwari, R.K. Sahu, A.K. Pramanick, Raghuvir Singh, Development of conversion coating on mild steel prior to sol gel nanostructured  $\text{Al}_2\text{O}_3$  coating for enhancement of corrosion resistance, *Surf. Coat. Technol.* 205 (2011) 4960-4967.
- D. Wang, G. P. Bierwagen, Sol-gel coatings on metals for corrosion protection, *Progress in Organic Coatings*, 64 (2009) 327-338.
- Yeh, T.-K.; Chien, Y.-C.; Wang, B.-Y.; Tsai, C.-H. Electrochemical Characteristics of Zirconium Oxide Treated Type 304 Stainless Steels of Different Surface Oxide Structures in High Temperature Water, *Corros. Sci.* 50 (2008), 2327-2337.

5. L. Curkovic, H. O. Curkovic, S. Salopek, M. M. Renjo, S. Šegota, Enhancement of corrosion protection of AISI 304 stainless steel by nanostructured sol-gel TiO<sub>2</sub> films, *Corrosion Science*, 77(2013) 76-81
6. C. X. Lei, H. Zhou, Z. D. Feng, Y. F. Zhu, R. G. Du , Low-temperature liquid phase deposited TiO<sub>2</sub> films on stainless steel for photogenerated cathodic protection applications, *Applied Surface Science*, 257 (2011) 7330-7334
7. G. X. Shen, Y. C. Chen, C. J. Lin , Corrosion protection of 316 L stainless steel by a TiO<sub>2</sub> nanoparticle coating prepared by sol-gel method, *Thin Solid Films*, 489, (2005) 130-136.
8. M. K. Sahnesarayi, H. Sarpoolaky, S. Rastegari ,Effect of heat treatment temperature on the performance of nano-TiO<sub>2</sub> coating in protecting 316L stainless steel against corrosion under UV illumination and dark conditions, *Surf. Coat. Technol.*, 258 (2014) 861-870.
9. E. Alat, A. T. Motta, R. J. Comstock, J. M. Partenzana, Multilayer (TiN, TiAlN) ceramic coatings for nuclear fuel cladding, *J. Nucl. Mater.*, 478 (2016) 236-244.
10. W. Cheng, Ch. Li. X Ma, L Yu, G. Liu, Effect of SiO<sub>2</sub>-doping on photogenerated cathodic protection of nano-TiO<sub>2</sub> films on 304 stainless steel, *Mater. & Design*, Vol 126, (2017) pp 155-161.
11. B.-H. Kim, S K. Nataraj, K. S. Yang, H.-G. Woo, Synthesis, characterization, and photocatalytic activity of TiO<sub>2</sub>/SiO<sub>2</sub> nanoparticles loaded on carbon nanofiber, *J. Nanosci. Nanotechnol.* 10 (2010) 3331-3335
12. A Ghasemi T Shahrabi A A Oskuie H Hassannehad and S Sanjabi, Effect of heat treatment on corrosion properties of sol-gel titania-ceria nanocomposite coating, *J. Alloys Comp.*, 504, (2010) 237-242